



Interconnection Feasibility Study Report

GIP-380-FEAS-R1

System Interconnection Request #380

50.22 MW Wind Generating Facility

Cumberland County (30N)

2012-02-01
Control Centre Operations
Nova Scotia Power Inc.

Executive Summary

The Interconnection Customer (IC) submitted an Interconnection Request (IR#380) for Network Resource Interconnection Service (NRIS) for a proposed 50.22 MW wind generation facility interconnected to the NSPI transmission system and also asked that Energy Resource Interconnection Service (ERIS) be studied concurrently. The Point of Interconnection (POI) requested by the customer is on the 69kV bus at the 30N-Maccan substation via approximately 14 km of newly-constructed line from the wind farm located near Minudie. An alternative POI identified by the IC is on the 138 kV bus at the 30N-Maccan substation.

In addition to the proposed generating facility, there are a Transmission Service Request (TSR-100) and two Interconnection Requests (IR#225 and IR#234) that are higher queued and will have an impact on the projects in northern Nova Scotia. TSR-100 has an in-service date of 2016 and both IR#225 and IR#234 have an in-service date of 2017, whereas IR#380 has an in-service date of early 2015. Therefore the FEAS for this IR is performed twice – for 2015 without TSR-100, IR#225 and IR#234 in service and again for 2017 with them in-service.

Under the existing “Import Power Monitor” Special Protection System (SPS) arming level, the flow on L-6513 could be at its conductor thermal limit during summer when 345 kV line L-8001 trips for any reason. With the addition of IR#380 loss of L-8001 could cause L-6513 to be overloaded up to 165% of its conductor thermal ratings during periods when summer line ratings are in effect, assuming other generation in this area is concurrently generating at full output. The overloads would also depend on the real-time local load demands and other local generation output. Therefore in order to accommodate IR#380 as NRIS this study recommends that L-6513 should be up-rated and that some terminal equipment upgrades be completed at 1N-Onslow and 74N-Springhill. The cost of uprating L-6513 will depend on the number of structures and spans that need to be remedied, but an estimate of the cost ranges from \$8.2M for thermal uprating to \$19.2M for complete rebuild. This study assumes that L-6513 can be up-rated for IR#380.

The “Import Power Monitor” SPS will no longer be needed under normal system conditions once the system upgrades associated with TSR-100 are completed in 2016. IR#380 could therefore operate without restrictions assuming that L-6513 is up-rated in 2015.

As ERIS with no transmission up-rate of L-6513, IR#380 would require the establishment of operating restrictions to curtail this wind facility whenever NS is importing 30-100MW from NB while summer conductor thermal ratings are in effect. The restrictions would also depend on the real-time local load demands and other local generation output besides NS Import/Export level. This operating restriction would no longer be needed after the upgrades associated with TSR-100 are in service. However there would also be operating restrictions required during the period when summer line ratings are in effect while NS imports above 600MW due to TSR-100 in 2016. When NS imports above 600 MW, loss of one 345 kV transmission line from New Brunswick will cause L-6513 to exceed its conductor thermal limits. Therefore IR#380 would have to be curtailed or the NS Import has to be reduced in order to avoid further transmission expansion requirements.

Utilization of the alternative POI on the 138 kV bus at 30N-Maccan substation shows similar results to those of the primary POI on the 69kV bus.

Control Centre Operations – Interconnection Feasibility Optional Study Report

To provide service reliability to customers in the area of Pugwash, Oxford, Springhill and Amherst, the 138/69 transformers at 30N-Maccan and 74N-Springhill provide alternate sources for the 69 kV system in the event that one transformer should fail or have to be removed from service for maintenance. Should the 30N-Maccan 138/69 kV transformer fail or be removed from service for maintenance then Springhill, Oxford and Pugwash would be supplied from the 74N-Springhill 138/69kV transformer via L-5029. Under these conditions, the addition of IR#380 onto 69 kV bus at 30N-Maccan would overload L-5029 and 74N-T61. Similarly, the 30N-Maccan 138/69 kV transformer would be overloaded due to the addition of this generating facility when the 74N-Springhill transformer is out of service. Although transformer failures are infrequent they have a long repair/replacement period (6-18 months). Therefore with IR#380 interconnecting onto the 69kV during such a period the generation output of this facility would be restricted to no more than 36 MW. The restriction would not be required for the POI on the 138kV bus.

No concern regarding short-circuit was found for this project on its own. Available flicker coefficient data for this type of machine indicates that voltage flicker will not be a problem. The project design must meet NSPI requirements for low-voltage ride-through, reactive power range and voltage control system. Based on the provided power factor of the GE XLE 1.62 MW (0.90), and the provided impedances of the transformers, supplementary reactive support may be needed in the form of capacitor banks at the low voltage terminals of the Interconnection Transformer. Harmonics must meet the Total Harmonics Distortion provisions of IEEE 519.

The preliminary value for the unit loss factor is calculated to be 5.4% for POI on 69 kV and 4.2% for POI on 138 kV (system losses increased by net 2.7 MW when IR #380 interconnects into 69 kV systems and 2.1 MW when IR#380 interconnects into 138 kV systems at the full output of 50.22 MW).

The preliminary non-binding cost estimate for interconnecting 50.22 MW onto 69 kV bus at 30N-Maccan substation would be \$15.2M as NRIS and \$5.8M as ERIS with operating restrictions. Both cost estimates include a contingency of 10% and they will be further refined in the System Impact Study and the Facility Study.

Table of Contents

	Page
Executive Summary	ii
1 Introduction	1
2 Scope	1
3 Assumptions	2
4 Projects with Higher Queue Positions	3
5 Objective	4
6 Short-Circuit Duty	5
7 Voltage Flicker and Harmonics	5
8 Thermal Limits.....	6
9 Voltage Limits.....	8
10 System Security /Bulk Power Analysis	9
11 Expected Facilities Required for Interconnection	9
12 NSPI Interconnection Facilities and Network Upgrades Cost Estimate	10
13 Issues to be addressed in SIS.....	12

1 Introduction

The Interconnection Customer (IC) submitted an Interconnection Request (IR#380) for Network Resource Interconnection Service (NRIS) for a proposed 50.22 MW wind generation facility interconnected to the NSPI transmission system and also asked that Energy Resource Interconnection Service (ERIS) be studied concurrently. The Point of Interconnection (POI) requested by the customer is on the 69kV bus at the 30N-Maccan substation via approximate 14 km of newly-constructed line from the wind farm located near Minudie. An alternative POI identified by the IC is on the 138 kV bus at the 30N-Maccan substation.

The Interconnection Customer (IC) signed a Feasibility Study Agreement to study the connection of their proposed generating facility to the NSPI transmission system dated 2011-12-21, and this report is the result of that Study Agreement. This project is listed as Interconnection Request #380 in the NSPI Interconnection Request Queue, and will be referred to as IR#380 throughout this report.

2 Scope

This Interconnection Feasibility Study (FEAS) consists of a power flow and short circuit analysis. Based on this scope, the FEAS report shall provide the following information:

1. Preliminary identification of any circuit breaker short circuit capability limits exceeded as a result of the interconnection;
2. Preliminary identification of any thermal overload or voltage limits violations resulting from the interconnection;
3. Preliminary description and high level non-binding estimated cost of facilities required to interconnect the Generating Facility to the Transmission System and to address the identified short circuit and power flow issues.

The Scope of this FEAS includes modeling the power system in normal state (with all transmission elements in service) under anticipated load and generation dispatch conditions.

In accordance with Section 3.2.1.2 of Standard Generation Interconnection Procedures (GIP), as approved by the UARB on February 10, 2010, the FEAS for ERIS consists of short circuit/fault duty, steady state (thermal and voltage) analyses. The short circuit/fault duty analysis would identify direct Interconnection Facilities required and the Network Upgrades necessary to address short circuit issues associated with the Interconnection Facilities. The steady state studies would identify necessary upgrades to allow full output of the proposed Generating Facility and would also identify the maximum allowed output, at the time the study is performed, of the interconnecting Generating Facility without requiring additional Network Upgrades. It is therefore assumed that transmission interfaces limits will not be exceeded to avoid system upgrades in an ERIS study.

In accordance with Section 3.2.2.2 of the GIP, the Interconnection Study for NR Interconnection Service shall assure that the Interconnection Customer's Generating Facility meets the requirements for NR Interconnection Service and as a general matter, that such Generating Facility's interconnection is also studied with the Transmission Provider's Transmission System at peak load, under a variety of severely stressed conditions, to determine whether, with the Generating Facility at full output, the aggregate of generation in the local area can be delivered to the aggregate of load on the Transmission Provider's Transmission System, consistent with the Transmission Provider's reliability criteria and procedures.

A more detailed analysis of the technical implications of this development will be included in the System Impact Study (SIS) report. The SIS includes system stability analysis, power flow analysis such as single contingencies (including contingencies with more than one common element), off-nominal frequency operation, off-nominal voltage operation, low voltage ride through, harmonic current distortion, harmonic voltage distortion, system protection, special protection systems (SPS), automatic generation control (AGC) and islanded operation. The impacts on neighbouring power systems and the requirements set by reliability authorities such as Northeast Power Coordinating Council (NPCC), North American Electric Reliability Corporation (NERC), and NSPI will be addressed at that time and will include an assessment of the status of the Interconnection Facility as a Bulk Power System element. The SIS may identify and provide a non-binding estimate of any additional interconnection facilities and/or network upgrades that were not identified in this FEAS.

An Interconnection Facilities Study follows the SIS in order to ascertain the final cost estimate to interconnect the generating facility.

3 Assumptions

This FEAS is based on the technical information provided by the Interconnection Customer. The Point of Interconnection (POI) and configuration is studied as follows:

1. Network Resource Interconnection Service and Energy Resource Interconnection Service types per section 3.2 of the GIP.
2. 50.22 MW wind with 31 units of GE XLE-1.62 MW Wind Turbines.
3. The generation technology used must meet NSPI requirement for reactive power capability of 0.95 capacitive to 0.95 inductive at the HV terminals of the IC Substation Step Up transformer. It is also required to have high-speed Automatic Voltage Regulation to maintain constant voltage at the generator terminals during and following system disturbances as determined in the subsequent System Impact Study.
4. The IC indicated that the generation interconnection point is on the 69 kV bus at 30N-Maccan substation via approximate 14 km of newly-constructed line from the wind farm. The alternative POI identified by the IC is on the 138 kV bus at 30N-Maccan.

5. Preliminary data was provided by the IC for the generator step-up and IC substation step-up transformers. Modeling was conducted with a 69kV-34.5kV 35/45/55 MVA Interconnection Facility transformer with a positive sequence impedance of 8% and an X/R ratio of 50. The IC indicated that this Interconnection Facility step-up transformer has a grounded wye-delta-wye winding configuration with +/-5% off-load tap changer. The impedance of generator step-up transformers is indicated to be 5.75% on 1.8 MVA with an assumed X/R ratio of 7.5.
6. The FEAS analysis is based on the assumption that IR's higher in the Generation Interconnection Queue and OATT Transmission Service Queue that have completed a System Impact Study, or that have a System Impact Study in progress will proceed, as listed in Section 4 below.

4 Projects with Higher Queue Positions

All in-service generation is included in the FEAS.

As of 2012-01-26 the following projects are higher queued in the Interconnection Request Queue and OATT Transmission Service Queue, and have the status indicated.

Interconnection Requests -Included in FEAS

- IR #8 GIA Executed
- IR #45 GIA Executed
- IR #56 GIA Executed
- IR #151 GIA Executed
- IR #219 GIA Executed
- IR #227 GIA in Progress
- IR #225 GIA in Progress
- IR #234 FAC in Progress

Interconnection Requests –Not Included in FEAS

- IR #131 SIS Milestones Met
- IR #360 SIS in progress
- IR #362 SIS in progress

OATT Transmission Service Queue– Included in FEAS

- TSR-100 SIS in progress

OATT Transmission Service Queue– Not Included in FEAS

- TSR-400 SIS Agreement Completed

While TSR-100, IR#225 and IR#234 are higher queued than IR#380, TSR-100 has an in-service date of 2016 and both IR#225 and IR#234 have an in-service date of 2017; whereas IR#380 has an in-service date of early 2015. Therefore the FEAS for this IR will

Control Centre Operations – Interconnection Feasibility Optional Study Report

be performed twice – for 2015 without TSR-100, IR#225 and IR234 in service and again for 2017 onwards with them in-service, along with any related system changes.

The additional Transmission Service Request TSR-400 and Interconnection Requests IR#131, IR#360 and IR#362 are higher queued than IR#380 and SISs are either in progress or about to be initiated. However, the results of these SISs are not sufficiently defined to be included in the FEAS for IR#380.

The following IRs either have SIS Agreements complete (but have not yet met the RGIP SIS progression milestones), or have Feasibility Study agreements complete. As such, they are not included in this FEAS.

IR #67	IR #68	IR#117	IR #126	IR #128	IR #149
IR #163	IR #213	IR #222	IR #235	IR #238	IR #241
IR #242	IR #314	IR #356	IR#364	IR#365	IR#367
IR#368	IR#374	IR#375	IR#372	IR#373	IR#378
IR#379	IR#361				

If any of the higher-queued projects included in this FEAS are subsequently withdrawn from the Queue, the results of this FEAS may require updating or a re-study may be necessary. The re-study cost incurred as a result of the withdrawal of the higher-queued project shall be the responsibility of the Interconnection Customer that withdraws the higher queued project.

5 Objective

The objective of this FEAS is to provide a preliminary evaluation of the system impact and the high-level non-binding cost estimate of interconnecting the 50.22 MW generating facility to the NSPI transmission system at the designated location. The assessment will identify potential impacts on the loading of transmission elements, which must remain within their thermal limits. Any potential violations of voltage criteria will be identified and addressed. If the proposed new generation increases the short-circuit duty of any circuit breakers beyond their rated capacity, the circuit breakers must be upgraded. Single contingency criteria¹ are applied for both NRIS and ERIS assessments.

This FEAS is based on a power flow and short circuit analysis and does not include a complete determination of facility changes/additions required to increase system transfer capabilities that may be required to the Bulk Power System to meet the design and operating criteria established by NPCC and NERC or required to maintain system stability. These requirements will be determined by the subsequent interconnection System Impact Study (SIS).

¹ The Single Contingency Criteria is defined by NPCC in its A-7 Document, and may involve more than one transmission element.

6 Short-Circuit Duty

The maximum (design) expected short-circuit level is 5000 MVA on 138kV systems and 3500 MVA on 69 kV systems. The short-circuit levels in the area before and after this development (including TSR-100) are provided below in Table 6-1.

Table 6-1: Short-Circuit Levels. Three-phase MVA ⁽¹⁾		
Location	IR #380 in service	IR #380 not in service
All transmission facilities in service		
30N-Maccan 69 kV (POI)	542	368
30N-Maccan 138 kV	1230	1100
74N-Springhill 138 kV	1313	1224
1N-Onslow 138 kV	2462	2441
Minimum Conditions		
30N-Maccan 69 kV (POI)	475	302

⁽¹⁾ Classical fault study, flat voltage profile

In determining the maximum short-circuit levels with this generating facility in service the generators have been modeled as conventional machines with reactance comparable to induction machines regardless of the type of generators proposed, which provides a worst case scenario. The SIS will refine the fault level based on the actual machine characteristics.

The maximum short-circuit level at the POI on the 69 kV bus at 30N-Maccan substation will be 368 MVA in 2016. With IR # 380 the increase will bring the short-circuit level to 542 MVA at the POI. Similarly, under summer light load conditions with certain generation units offline and certain lines out-of-service, the minimum short-circuit level will be approximately 302 MVA at the POI. This translates into maximum equivalent system impedance at the POI of 0.331 per unit on 100 MVA base.

The interrupting capability of the 138kV circuit breakers is at least 3500 MVA at 1N-Onslow, 5000 MVA at 74N-Springhill and 3000 MVA at 30N-Maccan. The interrupting capability of the 69kV circuit breakers is at least 3500 MVA at 74N-Springhill and 1000 MVA at 30N-Maccan substation. As such, the interrupting ratings will not be exceeded by this development on its own. Therefore IR#380 will not impact the circuit breakers at these stations.

7 Voltage Flicker and Harmonics

Due to the lack of flicker coefficient information on the GE 1.6-XLE machine, this study assumes the same flicker data as for the GE 1.5SLE machine. The calculated voltage flicker at the POI using IEC Standard 61400-21 and the published values for GE 1.5 SLE

that one transformer should fail or have to be removed from service for maintenance. Should the 30N-Maccan 138/69 kV transformer fail or be removed from service for maintenance then Springhill, Oxford and Pugwash would be supplied from the 138/69 kV transformer at 74N-Springhill via L-5029. Under these conditions, the addition of this generation project on the 69 kV at 30N-Maccan will overload L-5029 and 74N-T61. Similarly, the 30N-Maccan transformer will be overloaded due to the addition of this generating facility when 74N-Springhill 138/69 kV transformer is out of service. Although transformer failures are infrequent they have a long repair/replacement period (6-18 months). During such a period the operation of this facility would be restricted to no more than 36 MW. The restriction would not be required for the alternative POI on the 138kV bus.

Any new generating facilities added to the system in northern Nova Scotia (between Truro and New Brunswick) could have an impact on the transfer capability between Nova Scotia and New Brunswick and on the associated SPSs. The NSPI transmission line ratings records show that L-6513 between 74N-Springhill and 1N-Onslow substation is built with 556 ACSR Dove conductors with a maximum operating temperature of 50°C and a Summer/Winter line rating of 110/165 MVA limited by conductor sag with the restriction of 172 MVA due to the metering at both line terminals and the protection at 1N-Onslow end. Under the existing “Import Power Monitor” SPS arming level, the flow on L-6513 could be at its conductor thermal limit during the period when summer line ratings are in effect when 345 kV line L-8001 trips for any reason. With the addition of IR#380 loss of L-8001 could cause L-6513 to be overloaded up to 165% of its conductor thermal ratings during periods when summer line ratings are in effect, assuming other generation in this area is concurrently generating at full output. The overloads would also depend on the real-time local load demands and other local generation output. Therefore in order to accommodate IR#380 as NRIS this study recommends that L-6513 should be up-rated and that some terminal equipment upgrades associated with L-6513 be completed at 1N-Onslow and 74N-Springhill. The cost of uprating L-6513 will depend on the number of structures and spans that need to be remedied, but an estimate of the cost ranges from \$8.2M for thermal uprating to \$19.2M for complete rebuild. This study assumes that L-6513 can be up-rated for IR#380 and the associated cost estimates are listed in Section 12.

TSR-100 involves a request for a NS import from New Brunswick of 320 MW (firm) plus 400 MW (non-firm) with an in-service date of 2016. System network upgrades associated with TSR-100 include:

- New 345 kV transmission line from Coleson Cove, NB to Salisbury, NB
 - New 345 kV transmission line from Salisbury NB to Memramcook, NB
 - New 345 kV transmission line from Memramcook, NB to Onslow NS
 - Switched capacitor banks in NB at Memramcook, Salisbury and Norton
 - Static Var Compensators (SVC) in NB at Salisbury and Memramcook
- Once these upgrades are completed, the “Import Power Monitor” SPS may not be needed under normal system conditions. IR#380 can therefore operate without restrictions assuming that L-6513 is up-rated in 2015.

As ERIS with no transmission up-rate of L-6513, IR#380 would require the establishment of operating restrictions to curtail this wind facility whenever NS is importing 30-100MW from NB while summer conductor thermal ratings are in effect. The restrictions would also depend on the real-time local load demands and other local generation output besides NS Import/Export level. This operating restriction would no longer be needed after TSR-100 is in service. However there would also be operating restrictions required during the period when summer line ratings are in effect while NS imports above 600MW due to TSR-100 after 2016. When NS imports above 600 MW, loss of one 345 kV transmission line from New Brunswick will cause L-6513 to exceed its conductor thermal limits. Therefore IR#380 would have to be curtailed or the NS Import has to be reduced in order to avoid further transmission expansion requirements.

Utilization of the alternative POI on the 138 kV bus at 30N-Maccan substation shows similar results to those of the primary POI on the 69kV bus.

The SIS will determine the detailed system requirements to accommodate IR#380. The requirement for restrictions or curtailments of this facility when operating with an element (transmission line, transformer etc) out of service (N-1 operation) will be further assessed in the SIS.

9 Voltage Limits

This project, like all new generating facilities must be capable of providing both lagging and leading power factor of 0.95, measured at the HV terminals of the IC Substation Step Up Transformer, at all production levels up to the full rated load of 50.22 MW. Data provided by the IC indicates that IR#380 may not be able to meet this requirement without additional reactive support. Based on the assumed rated power factor of the GE XLE-1.62 MW (0.9), and the provided impedances of the transformers, supplementary reactive support may be needed in the form of capacitor banks at the low voltage terminals of the Interconnection Transformer. This will be further investigated in the System Impact Study. More information on a potential tap-changer will be required for that analysis.

A centralized controller will be required which continuously adjusts individual generator reactive power output within the plant capability limits and regulates the voltage at the 34.5 kV bus voltage. The voltage controls must be responsive to voltage deviations at the terminals of the Interconnection Facility substation, be equipped with a voltage set-point control, and also have the ability to slowly adjust the set-point over several (5-10) minutes to maintain reactive power within the individual generators capabilities. The details of the specific control features, control strategy and settings will be reviewed and addressed in the SIS, as will the dynamic performance of the generator and its excitation.

The NSPI System Operator must have manual and remote control of the voltage set-point and the reactive set-point of this facility to coordinate reactive power dispatch requirements.

This facility must also have low voltage ride-through capability as per Appendix G of the Standard Generator Interconnection and Operating Agreement (GIA). The SIS will state specific options, controls and additional facilities that are required to achieve this.

10 System Security /Bulk Power Analysis

There are a number of proposed generation additions in New Brunswick that may have an impact on projects in northern NS and vice versa. Their POI, size and relative position of the NS and NB interconnection Queues will determine the impact. This will be resolved through collaboration with NBSO at the SIS stage.

As NRIS this generating facility will also increase loading on the Onslow South corridor (Truro to Halifax) by replacing generation located south and west of Truro. This may require increased reactive support in the Halifax area or invoke facility additions that can reduce the reactive support requirements. This will be evaluated in the SIS.

The SIS will determine if any facility changes are required to permit the proposed higher transmission loadings while maintaining compliance with NERC/NPCC standards and in keeping with good utility practice.

11 Expected Facilities Required for Interconnection

The following facility changes are required to interconnect IR #380 onto the 69kV bus at 30N-Maccan substation:

Additions/Changes for POI on the 69 kV bus at 30N-Maccan:

1. Addition of approximately 14 km of newly-constructed transmission line from POI to customer substation consisting of 556 Dove ACSR conductor rated 100°C conductor temperature,
2. A dedicated 69 kV circuit breaker and associated switches at 30N for the spur line to the wind farm,
3. Modification on NSPI protection systems,
4. Control and communications between the wind farm and NSPI SCADA system (to be specified).
5. Up-rate L-6513 (65 km) and upgrade the line terminals as required for NRIS type.

Requirements for the Generating Facility

1. 69 kV Interconnection Substation. This will include a circuit breaker at high side of customer power transformer and protections as acceptable to NSPI. An RTU to interface with NSPI's SCADA, with telemetry and controls as required by NSPI.

2. Facilities to provide 0.95 leading and lagging power factor when delivering rated output at the HV terminals of the IC Substation Step Up Transformer when the voltage at that point is operating between 95 and 105 % of nominal.
3. Centralized controls. These will provide centralized voltage set-point controls and are known as Farm Control Units (FCU). The FCU will control the 34.5 kV bus voltage and the reactive output of the machines. Responsive (fast-acting) controls are required. The controls will also include a curtailment scheme which will limit or reduce total output from the facility, upon receipt of a telemetered signal from NSPI's SCADA system.
4. NSPI to have control and monitoring of reactive output of this facility, via the centralized controller. This will permit the NSPI Operator to raise or lower the voltage set-point remotely.
5. Low voltage ride-through capability as per Appendix G to the Standard Generator Interconnection and Operating Agreement (GIA).
6. Real-time monitoring (including a Remote Terminal Unit) of the interconnection facilities.
7. Facilities for NSPI to execute high speed rejection of generation (transfer trip) if determined in SIS.

12 NSPI Interconnection Facilities and Network Upgrades Cost Estimate

Estimates for NSPI Interconnections Facilities and Network Upgrades for interconnecting 50.22 MW wind energy onto the 69 kV systems with NRIS are included in Table 12-1, and ERIS in Table 12-2.

Control Centre Operations – Interconnection Feasibility Optional Study Report

Table 12-1: Cost Estimates identified from FEAS scope for NRIS		
	Determined Cost Items	Estimate
NSPI Interconnection Facilities		
i	Build 14 km 69kV single circuit line into the 30N substation	\$ 4,060,000
ii	69 kV circuit breakers& associated switches and the new line terminal into 30N-Maccan	\$ 530,000
iii	Protection, control, communication	\$700,000
Network Upgrades		
iv	Up-rate L-6513 (65 km)	\$8,125,000
v	Upgrade line terminals of L-6513 (protection & metering)	\$400,000
Totals		
vi	Contingency (10%)	\$1,381,500
vii	Total of Determined Cost Items	\$15,196,500
To be Determined Costs		
viii	System additions to address potential stability limits	TBD (SIS)

Table 12-2: Cost Estimates identified from FEAS scope for ERIS		
	Determined Cost Items	Estimate
NSPI Interconnection Facilities		
i	Build 14 km 69kV single circuit line into the 30N substation	\$ 4,060,000
ii	69 kV circuit breakers& associated switches and the new line terminal into 30N-Maccan	\$ 530,000
iii	Protection, control, communication	\$700,000
Totals		
vi	Contingency (10%)	\$529,000
vii	Total of Determined Cost Items	\$5,819,000
To be Determined Costs		
viii	System additions to address potential stability limits	TBD (SIS)

The preliminary non-binding cost estimate for interconnecting 50.22 MW onto 69 kV bus at 30N-Maccan substation as NRIS would be \$15,196,500 including a contingency of 10%. The Interconnection Customer is also required to fund the Items iv) and v) costs, but would be eligible for repayment in accordance with the terms of the GIA.

The preliminary non-binding cost estimate for interconnecting IR#380 into the 30N-Maccan substation with operating restrictions as ERIS would be \$5,819,000 including a contingency of 10%, and the cost estimates does not include the network upgrades on L-6513.

13 Issues to be addressed in SIS

The following provides a preliminary scope of work for the subsequent SIS for IR#380. The SIS will include a more comprehensive assessment of the technical issues and requirements to interconnect generation as requested. It will include contingency analysis, system stability and ride through and operation following a contingency (N-1 operation). The SIS must determine the facilities required to operate this facility at full capacity, withstand any contingencies (as defined by the criteria appropriate to the location) and identify any restrictions that must be placed on the system following a first contingency loss. The SIS will confirm the options and ancillary equipment that the customer must install to control flicker, voltage and ensure that the facility has the required ride-through capability. The SIS will be conducted in accordance with the GIP with the assumption that all appropriate higher-queued projects will proceed and the facilities associated with those projects are installed.

The following outline provides the minimum scope that must be complete in order to assess the impacts. It is recognized the actual scope may deviate, to achieve the primary objectives.

The assessment will consider but not be limited to the following.

- i. Facilities that the customer must install to meet the requirements of the GIP
- ii. The minimum transmission additions/upgrades that are necessary to permit operation of this Generating Facility, under all dispatch conditions, catering to the first contingencies listed.
- iii. Guidelines and restrictions applicable to first contingency operation (curtailments etc)
- iv. System loss impacts
- v. Under-frequency load shedding impacts

To complete this assessment the following first contingencies, as a minimum, will be assessed:

- L-8001/3025
- L-3006 – with and without NBPT SPS operation
- Memramcook 345/138 kV transformer
- L-6513
- L-6514
- L-6535/L-1159
- L-6536/L-1160
- L-8003
- L-8002 & L-8003 (common circuit breaker)
- L-8003 & L-8004 (common circuit breaker)
- L-8001 & 67N-T81 TX (common circuit breaker)

Control Centre Operations – Interconnection Feasibility Optional Study Report

- L-8002 & 67N-T81 TX (common circuit breaker)
- L-3006 & L-3025 & Memramcook 345/138 kV Tx (common breaker)
- L-3006 & L3017 (common breaker)
- 1N-B61
- L-1108/1190 Common 138kV structure
- Loss of 180 MW of load under peak load conditions and 250 MW under light load conditions
- Loss of largest generation – Pt. Aconi 174MW net
- Loss of two generating units at Lingan – 312 Net
- Loss of the Trenton Bus (Two units with load)

To complete this assessment the dynamics of the following first contingencies, as a minimum, will be assessed:

- 3 phase fault L-8001/3025 at 67N-Onslow, NS Import SPS operation (islanding)
- 3 phase fault L-3006 at Memramcook, NB SPS/UVLS operation (islanding)
- 3 phase fault L-3006 at Salisbury, NB SPS/UVLS operation (islanding)
- 3 phase fault L-8003 at 67N-Onslow
- 3 phase fault L-8002 at 67N-Onslow
- Slg L-3017, drops L-3017&L-3006 (common CB), NB SPS/UVLS operation,
- Slg Memramcook T3, drops L-3006 (common CB), NB SPS/UVLS operation
- Slg L-8002 at Onslow, drops L-8003, Grp5 SPS Operation
- 3 phase fault at 79N-Hopewell, drops L-8003, 8004, bus, SPS operation
- 3 phase fault 1N-Onslow 138 kV bus B61
- 3 phase fault 74N-Springhill 138 kV bus

Any changes to SPS schemes required for operation of this generating facility, in addition to existing generation and facilities that can proceed before this project, will be determined by the SIS as well as any required additional transmission facilities. The determination will be based on NERC² and NPCC³ criteria as well as NSPI guidelines and good utility practice. The SIS will also determine the contingencies for which this facility must be curtailed.

The SIS will calculate the unit loss factor, which is a measure of the percentage of the net output of IR #380 which is lost through the transmission system. The preliminary value for the unit loss factor is calculated to be 5.4% for POI on 69 kV and 4.2% for POI on 138 kV (system losses increased by net 2.7 MW when IR #380 is operated at 69 kV and 2.1 MW when IR#380 is operated at 138 kV with 50.22 MW output).

Nova Scotia Power
2012-02-01

² NPCC criteria are set forth in it's Reliability Reference Directory #1 *Design and Operation of the Bulk Power System*

³ NERC transmission criteria are set forth in *NERC Reliability Standards TPL-001, TPL-002, TPL-003*